Compact High-Performance Continuous-Wave Double-Resonance Rubidium Standard With $1.4 \times 10^{-13} \ \tau^{-1/2}$ Stability

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Abstract—We present our studies on a compact high-performance continuous wave (CW) double-resonance (DR) rubidium frequency standard in view of future portable applications. Our clock exhibits a short-term stability of 1.4 \times 10⁻¹³ τ ^{-1/2}, consistent with the short-term noise budget for an optimized DR signal. The metrological studies on the medium- to longterm stability of our Rb standard with measured stabilities are presented. The dependence of microwave power shift on light intensity, and the possibility to suppress the microwave power shift is demonstrated. The instabilities arising from the vapor cell geometric effect are evaluated, and are found to act on two different time scales (fast and slow stem effects). The resulting medium- to long-term stability limit is around 5.5 imes 10^{-14} . Further required improvements, particularly focusing on medium- to long-term clock performance, are discussed.

I. Introduction

YOMPACT rubidium (Rb) frequency standards form the backbone of today's satellite navigation systems [1]. Recently developed laser-pumped Rb cell standards exhibit short-term frequency stabilities at least one order of magnitude better than the commercial lamp-pumped standards [2], [3].

We are developing a compact laser-pumped high-performance Rb cell standard exhibiting the performances of a passive H-maser [4], but with a reduced volume (by a factor of <10), mass (by a factor of <5) and power consumption (by a factor of <4). Our Rb cell standard is based on the continuous-wave (CW) double-resonance (DR) principle [5], [6]. The CW DR spectroscopy involves two resonant electromagnetic fields that are operated simultaneously to interrogate the atoms—the optical field to polarize the atoms by optical pumping, and the microwave

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field to drive the ground-state hyperfine clock transition that serves as an atomic frequency reference. This CW approach is simple in its operation and requires no acoustooptical modulators (AOM), unlike a pulsed-optical pumping (POP) scheme, and has lower design complexity than cold atom clocks, thereby also reducing the volume of the clock. The POP method has stringent requirements on the microwave local oscillator phase noise, but these requirements are less stringent in the CW method. Furthermore, rubidium standards have been tested for reliability in onboard satellite- and deep-space navigation systems [7].

This paper is divided into following sections. Section II explains the details of the experimental setup. Section III gives the details on the DR signal and short-term stability noise budget. A systematic metrological characterization of the physical effects perturbing the medium- to longterm clock frequency stability, such as the second-order Zeeman shift, light-shifts, microwave power shift, cavity pulling, spin-exchange shift, and the temperature coefficient shifts are presented in Section IV. In Section V, we estimate the limits resulting from the vapor cell geometric effect. In Section VI, we present the short-, medium-, and long-term frequency stabilities of our Rb standard. Finally, in Section VII conclusions are drawn, with future prospects required to improve our clock performances.

II. Experimental Setup

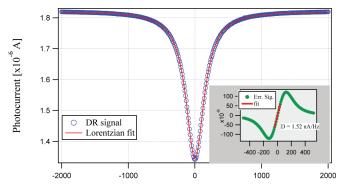
The details of our experimental clock setup were previously presented in [2] and [5]. The setup consists of three main components, 1) the frequency stabilized compact laser head (LH), with overall volume and mass of $<0.9 \text{ dm}^3$ and <0.6 kg, respectively; 2) the physics package (PP), with overall volume and mass of $<0.8 \text{ dm}^3$ and <1.4 kg, respectively; and 3) the low-noise microwave synthesizer (local oscillator, LO), which is presently a rack-mount device. The laser is a distributed feedback (DFB) diode emitting at 780 nm (Rb D2 transition). The laser is frequency stabilized using an evacuated Rb reference cell that is integrated in the LH assembly. Further details on the laser head were reported in [8]. The details on the PP were reported in [5], [6]. The core of this PP consists of a glass cell of 25 mm diameter that contains Rb vapor and a mixture of argon and nitrogen buffer gases with a pressure ratio of $P(Ar)/P(N_2) = 1.6$. Our Rb cell has two distinct parts: the cell volume, where the ⁸⁷Rb vapor is interro-

gated with laser and microwave to obtain the DR signal, and the cell stem that acts as a reservoir for metallic Rb. This cell is situated inside a newly developed compact magnetron-type microwave resonator (volume <45 cm³) [9]. This resonator assembly is mounted inside a solenoid (C-field coils) to lift the degeneracy of ⁸⁷Rb hyperfine ground states into their respective Zeeman levels, such that we can selectively interrogate the clock transition: 5 ${}^{2}S_{1/2} \mid F_{\rm g}=1, m_{\rm F}=0 \rangle \leftrightarrow \mid F_{\rm g}=2, m_{\rm F}=0 \rangle$ that has an unperturbed frequency of $\nu_{\rm Rb} = 6834682610.90429(9) \; {\rm Hz}$ [10]. This whole assembly is mounted inside two μ -metal magnetic shields to suppress perturbations caused by external magnetic field fluctuations (cf. Section IV-A). The LO module consists of an oven controlled crystal oscillator (OCXO) and the microwave synthesis chain to generate ~6.835 GHz for ⁸⁷Rb clock transition interrogation. The phase noise of the LO was measured by the cross-correlation method. At a carrier frequency of 6.8 GHz, it has a noise level of −70 dB·rad²/Hz at 1 Hz Fourier frequency and a noise floor of $-111 \text{ dB} \cdot \text{rad}^2/\text{Hz}$ from 10^3 Hz to $2 \times$ 10⁴ Hz. Further details on the LO including the digital lock-in and clock loop electronics can be found in [3]. The signal that is detected using a photodetector situated at the exit of the PP is preamplified and fed to a synchronous detector that generates an error signal by operating at the modulation frequency $f_{\rm m}$ applied to the ${\sim}6.8~{\rm GHz}$ output frequency of the LO. This is used to lock the crystal oscillator to the atomic resonance frequency. The modulation depth is chosen to be $\delta = 100$ Hz, approximately 30% of the FWHM linewidth of the DR signal (see Fig. 1). Once the clock loop is closed, the stabilized 10 MHz output frequency from the LO module is compared with the 10 MHz signal from an active hydrogen maser and the frequency stability is recorded using a computer interface. Note that for the DR spectroscopy, the clock loop is not closed; instead, the output from the detector as a function of microwave frequency is directly monitored and recorded using an oscilloscope.

III. DR SIGNALS AND SHORT-TERM STABILITY NOISE BUDGET

Optimized DR signals shown in Fig. 1 were obtained for a laser intensity of 0.46 $\mu W/mm^2$ and a microwave input power of $-34~\mathrm{dBm}.$

The DR signal has an amplitude of 0.48 μ A, a background level of 1.82 μ A, a contrast of 26%, and a linewidth (FWHM, $\Delta\nu_{1/2}$) of 334 Hz. The theoretically estimated intrinsic linewidth of 350 Hz (due to collisional relaxations of buffer gases and cell walls, and the Rb-Rb spin-exchange relaxation) matches well with the measured value of $\Delta\nu_{1/2}=334$ Hz (cf. Fig. 1). The shift of the Rb-hyperfine center frequency $\nu_{\rm Rb}$ resulting from buffer gas pressure (2.6 kPa) is measured as 3390 Hz, this is in excellent agreement with theoretically estimated value of 3385 Hz. The error signal corresponding to the DR Lo-



Microwave detuning from 6.834686 GHz ($\nu'_{Rb} = \nu_{Rb} + 3390$ Hz) [Hz]

Fig. 1. DR spectroscopic signal with the 25 mm buffer gas cell. It exhibits an amplitude $A=0.48~\mu\mathrm{A}$, background level $Bk=1.82~\mu\mathrm{A}$ and contrast C=A/Bk=26% and linewidth $\Delta\nu_{1/2}=334~\mathrm{Hz}$. The microwave center frequency was set to 6.834686 GHz that is higher than ν_{Rb} by 3390 Hz due to a buffer gas pressure of 2.6 kPa. The inset shows the de-modulated error signal with a discriminator slope of $D=1.52~\mathrm{nA/Hz}$. The microwave synthesizer frequency is stabilized to the center of this curve.

rentzian is shown in the inset of Fig. 1. This is obtained by frequency modulating the microwave frequency in the closed clock-loop configuration.

The short-term stability of a passive rubidium frequency standard (1 to 100 s) limited by signal-to-noise (S/N) ratio can be estimated by the formula [2]

$$\sigma_{\rm S/N}(\tau) = \frac{N_{\rm psd}}{\sqrt{2} \cdot D \cdot \nu_{\rm Rb}} \cdot \tau^{-1/2},\tag{1}$$

where $N_{\rm psd}$ is the detection noise power-spectral-density when microwave and pump laser are switched on (in closed clock-loop condition) and D is the discriminator slope of the error signal. The measured noise density, $N_{\rm psd}$ also includes the contribution of PM-to-AM (phase noise to amplitude noise) laser noise conversion in the clock cell [11], [12].

The detection shot noise is estimated by considering the dc photocurrent, $I_{\rm dc} \sim 1.6~\mu{\rm A}$ at FWHM $(\Delta v_{1/2})$ of the DR signal by using the formula $N_{\rm shot} = \sqrt{2 \cdot e \cdot I_{\rm dc}}$, where e is the charge of an electron. Using (1), we then estimate a shot-noise-limited clock frequency stability of 4.9 × $10^{-14}~\tau^{-1/2}$. However, the short-term stability of our clock presently has an S/N limit of $\sim 1.2 \times 10^{-13}$, mainly due to FM-to-AM conversion of laser FM noise in the atomic vapor [11]. The resulting S/N budget limiting the short-term stability of our clock is presented in Table I.

The final limit, $\sigma_y(\tau)$, on short-term stability also must include the influences resulting from the intermodulation effects on the phase noise of the LO and the laser intensity and frequency fluctuations via the light-shifts (LS) (cf. Section IV-B). This can be estimated from sum of the squares of the individual limits by the equation

$$\sigma_{y}(\tau) = \sqrt{\sigma_{S/N}(\tau)^{2} + \sigma_{PMnoise}(\tau)^{2} + \sigma_{LS}(\tau)^{2}}.$$
 (2)

TABLE I. SHORT-TERM NOISE BUDGET OF THE 25-MM-CELL CLOCK.

Source	$\begin{array}{c} {\rm Noise} \\ ({\rm pA}/\sqrt{\rm Hz}) \end{array}$	Instability $\sigma_{\rm inst}(\tau) \ \tau^{-1/2}$
Detector noise	0.362	2.5×10^{-14}
Microwave noise	0.74	5.1×10^{-14}
Laser noise (microwave off)	1.46	1×10^{-13}
Total S/N (calculated)	1.68	1.15×10^{-13}
Total, S/N (measured) (clock loop noise)	1.7	1.17×10^{-13}

The additional instability arising from the LO PM noise because of the aliasing effect is estimated by the method described in [13]. At our clock modulation frequency $f_{\rm m}=44$ Hz, by considering the even harmonics up to 100 kHz, we estimate the contribution of the phase noise caused by the aliasing effect as $\sigma_y(\tau)=7.5\times 10^{-14}~\tau^{-1/2}$. The total contribution from the laser intensity and the frequency fluctuations via LS effect is estimated to be $\sigma_{\rm LS}=4\times 10^{-14}$, and from Table I, we have $\sigma_{\rm S/N}(\tau)=1.17\times 10^{-13}$. Substituting these values into (2), the overall short-term clock stability is estimated as $\sigma_y(\tau) \sim 1.4\times 10^{-13}~\tau^{-1/2}$.

IV. MEDIUM- TO LONG-TERM STABILITY STUDIES

Various physical perturbations affect the medium- to long-term clock stability. They were measured and evaluated, and are presented in this section.

A. Second-Order Zeeman Shift on Clock Transition

Although the clock transition is unaffected by the magnetic field in first-order, the second-order perturbations caused by magnetic field variations give rise to the second-order Zeeman shift [14], and can be written as [15]

$$\Delta \nu_{\rm Z} = A_0 |\mathbf{B} \cdot \hat{z}|^2$$
, with $A_0 = 575.14 \; {\rm Hz/G^2}$, (3)

where \hat{z} is the quantization axis direction. The magnetic field $\bf B$ includes the combination of contributions [15] from the applied quantization magnetic field $\bf B_0$, the residual field $\bf B_r$, and the field related to the noise of the magnetic shields $\bf B_s$. $\bf B_r$ is the field that remains even after the shields are used to suppress the magnitude of an external magnetic field fluctuations. The fluctuations of these terms on clock frequency can be characterized by their respective variances, $\sigma_{B_0}^2(\tau)$, $\sigma_{B_r}^2(\tau)$, and $\sigma_{B_s}^2(\tau)$ as [15]

$$\sigma_y^2(\tau) = \left(\frac{2A_0 \mathbf{B_0}}{\nu'}\right)^2 \{\sigma_{B_0}^2(\tau) + \sigma_{B_r}^2(\tau) + \sigma_{B_s}^2(\tau)\}. \tag{4}$$

Influence on clock instability is analyzed as follows. We apply, typically, a quantization field (C-field) of ${\bf B_0}\approx 40$ mG, and the measured relative stability of this field resulting from resonator control electronics is $\sigma_{\Delta B_0/B_0}(\tau) < 10^{-6}$ for time averages up to 10^5 s, which implies $\sigma_{B_0}(\tau) = 40$ nG. We measured a residual magnetic field ${\bf B_r}\approx 1.3$ mG at zero external field and with a measured shield-

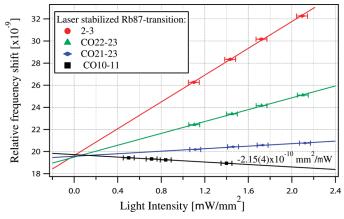


Fig. 2. Clock frequency shift as a function of laser intensity for the laser frequency stabilized to different Rb sub-Doppler transitions: 2–3: $|F_{\rm g}=2\rangle \rightarrow |F_{\rm e}=3\rangle$, CO22–23: $|F_{\rm g}=2\rangle \rightarrow |F_{\rm e}=2\rangle$, CO31–23: $|F_{\rm g}=2\rangle \rightarrow |F_{\rm e}=1\rangle$, CO21–23: $|F_{\rm g}=2\rangle \rightarrow |F_{\rm e}=1\rangle$, CO31–23: $|F_{\rm g}=2\rangle \rightarrow |F_{\rm e}=1\rangle$, Cross-Over, and CO10–11: $|F_{\rm g}=1\rangle \rightarrow |F_{\rm e}=0\rangle$, Cross-Over, transition.

ing factor of 3067, we estimate $\sigma_{B_{\rm r}}(\tau) \approx 0.4~\mu{\rm G}$. From [15] and [16], for our external shield with radius $r=49~{\rm mm}$ and thickness $t=0.8~{\rm mm}$, the influence resulting from the magnetic shield noise is estimated as $\sigma_{B_{\rm s}}(\tau) \approx 132~{\rm pG}$. From (4), and these values, the total influence resulting from magnetic variations on clock frequency resulting from second-order magnetic variation is $\sigma_y(\tau) \approx 2.7 \times 10^{-15}~{\rm up}$ to $\tau=10^5~{\rm s}$; however, this value could degrade to the level of 10^{-14} in perturbed geomagnetic conditions.

B. Intensity and Frequency Light Shifts (LS)

A theoretical description of the light shift (ac Stark shift) can be found in [17] and [18]. At a fixed laser frequency (i.e., when we stabilize our laser to a particular sub-Doppler transition), the clock frequency shift was measured as a function of the input laser intensity to get the intensity LS coefficient, α [18]. This method was repeated by stabilizing to different sub-Doppler transitions as shown and explained in Fig. 2. The clock frequency shift (y-scaling) is in relative frequency units, normalized to the nominal clock frequency. For the transition $|F_{\rm g}=1\rangle \rightarrow |F_{\rm e}=01{\rm Cross-Over}\rangle$, we measured the lowest intensity light shift coefficient, $|\alpha|=2.15\times 10^{-10}~{\rm mm^2/\mu W}=1.46~{\rm Hz\cdot mm^2/\mu W}.$

Furthermore, when the laser intensity was kept constant, the clock frequency shift was measured as a function of laser frequency, which gives the frequency LS coefficient, β [18].

By fixing the laser intensity, the value of β is evaluated as the slope of the line fits shown in Fig. 3(a). The frequency LS coefficient can be suppressed in the pulsed mode [19]. In the CW operation discussed here, it is not possible to completely suppress β , but the influence can be reduced by operating at low light intensities as shown in Fig. 3(b), with a linear dependence of β on $I_{\rm L}$. Our measurements showed that the dependence of β on laser input intensity has a slope of 184 mHz/MHz·mm²/ μ W.

TABLE II. SUMMARY OF INSTABILITY CONTRIBUTIONS FROM PHYSICAL PERTURBATIONS ON THE CLOCK TRANSITION FOR MEDIUM- TO LONG-TERM TIME SCALES.

Physical effect	Coefficient	Variation	Instability at $10^4 \mathrm{s}$
Intensity LS effect, $ \alpha $	1.47 Hz·mm ² /μW	$4.6 \times 10^{-5} \mu \text{W/mm}^2$	9.9×10^{-15}
Frequency LS effect, $ \beta $	82 mHz/MHz	<3.1 kHz	3.7×10^{-14}
Microwave PS, $ \mu_{PS} $	$15.3~\mathrm{mHz/\mu W}$	$0.4 imes 10^{-3}~\mu\mathrm{W}$	8.9×10^{-16}
Cell volume TC TC _v	$1 \times 10^{-12} / \text{K}$	$3.5~\mathrm{mK}$	3.5×10^{-15}
(linear fit)	·		
Cell volume TC TC _v	$4.34 \times 10^{-12}/\mathrm{K}^2$	$3.5~\mathrm{mK^2}$	5.3×10^{-17}
(quadratic fit)	•		
Stem TC TC _s	$1.22 \times 10^{-11} / \mathrm{K}$	$4.6~\mathrm{mK}$	5.6×10^{-14}
Spin exchange shift TC _{SE}	$< 5 \times 10^{-12} / \text{K}$	$\sim 5 \text{ mK}$	$< 2.3 \times 10^{-14}$
Cavity pulling $ \Delta \nu_{\rm CP} $	$< 3.2 \times 10^{-14} / \mathrm{K}$	$\sim 5 \text{ mK}$	$< 1.6 \times 10^{-16}$

The estimation is done at 10^4 s integration time.

At our input laser intensity $I_{\rm L}=0.46~\mu{\rm W/mm^2}$, we get a frequency LS coefficient value of $\beta=1.2\times10^{-17}~{\rm Hz^{-1}}$ (or 82 mHz/MHz), and its effect on clock frequency instability is evaluated in Table II.

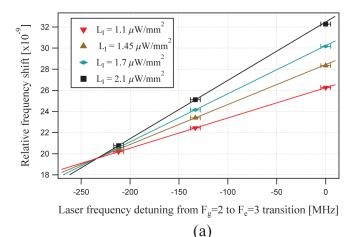
C. Microwave Power Shift and Dependence on Light Intensity

In the optical-microwave DR interrogation scheme using buffer-gas cells, the microwave power shift is an unavoidable phenomenon because the atoms are relatively well-confined in space during the microwave interaction, thereby causing the detected overall signal to be an inhomogeneous integration over the occurring spatial gradients [14], [20], [21]. It can be attributed to the microwave magnetic field distribution (spatial mode) inside the cavity. The observed shift is a weighted average of the ensemble of atoms that is dependent on each atom's position inside the cell. Therefore, in a buffer gas cell, the light shift varies along the path of the light beam—and possibly even across its profile—thereby causing inhomogeneous broadening and shifts of the resonance signal [14], that can also be influenced by residual gradients in the static magnetic c-field [22]. Hence, in a DR signal, we can say that the measured resonance frequency is a function of the applied microwave (RF) power. This inhomogeneity causes a shift on the clock hyperfine frequency and is termed the power shift, $|\mu_{\rm PS}|$. The observed shift is dependent on the light intensity and mimics the light shift behavior, known as the pseudo-light-shift effect [19]. Although the observed effects have been treated with numerical analysis and some theoretical approaches were undertaken [23], [24], a detailed theory that gives a complete picture still must be formalized. In this work, we focus our studies on evaluating the observed shift and its influence on the clock's stability.

The $\mu_{\rm PS}$ was measured in the following method. At each fixed microwave power injected to the cavity, the clock frequency shift was measured as a function of laser intensity. Then, the light-shift free value, meaning the pure microwave power shift value, was extracted by extrapolating to zero laser intensity, $I_{\rm L}$. These extracted shift values at each microwave input power are plotted in Fig. 4, the

slope $(-4 \times 10^{-13}/\text{dBm})$ gives the pure microwave power shift on the clock frequency. Its effect on medium- to long-term clock frequency is evaluated in Table II.

In addition, we evaluate the dependency of $|\mu_{\rm PS}|$ on the input light intensity. At a reduced intensity LS coefficient of 1.47 Hz·mm²/ μ W, the dependency of microwave PS coefficient (in Hz/dBm) on the interrogating light-intensity $I_{\rm L}$ is well pronounced, as shown in Fig. 5. For instance, at



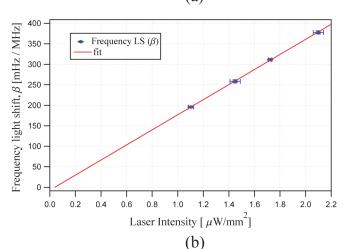


Fig. 3. (a) Clock frequency shift as a function of laser frequency, and (b) the frequency light-shift coefficient, β , as a function of input laser intensity.

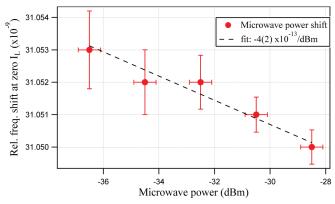


Fig. 4. Microwave power shift. The y-scaling shows relative frequency shift.

an input laser intensity of $\approx 0.1~\mu W/mm^2$, one can suppress the effect of microwave power shift in CW operation.

D. Temperature Coefficients (TCs)

Temperature dependence in buffer gas vapor cells arises because of the 87 Rb-buffer gas collisions [14]. A mixture of buffer gases can be used to reduce the temperature coefficient. We use an appropriate mixture of argon (Ar) and nitrogen (N₂) as buffer gases. While N₂ produces the necessary fluorescence quenching, Ar counter-balances the TC of nitrogen. Moreover, Ar has a negative linear temperature coefficient, whereas nitrogen has a positive linear temperature coefficient and because of their (much smaller) quadratic temperature coefficients, the mixture of these two at a certain temperature can give, in principle a zero (or inversion point) temperature coefficient [14], [25]. The equation that dictates this methodology can be written as [14], [25]

$$\Delta \nu_{\rm BG}(T) = \nu_{\rm Rb} + P_{\rm t}(\beta' + \delta' \Delta T + \gamma' \Delta T^2), \qquad (5)$$

where $P_{\rm t} = P_{N_2} + P_{\rm Ar}$ is the total gas pressure, and $\Delta T = T - T_0$ is the difference between the working temperature

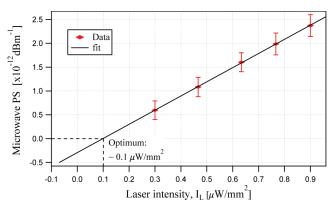


Fig. 5. Microwave power shift dependence on the input laser intensity. \blacksquare

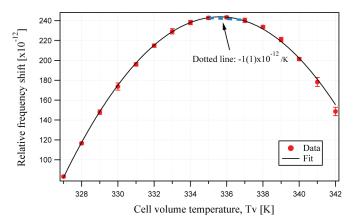


Fig. 6. Temperature coefficient of the cell volume.

and the reference temperature for which the coefficients are measured. Note that the total gas pressure $P_{\rm t}$ might vary during the cell sealing [25]. $\beta',\,\delta',\,\gamma'$ are the pressure coefficient, the linear temperature coefficient, and the quadratic temperature coefficient of the mixture, respectively, for the gas mixture. Furthermore, $\beta'=(\beta_{\rm N_2}+r\beta_{\rm Ar})/(1+r),\,\delta'=(\delta_{\rm N_2}+r\delta_{\rm Ar})/(1+r),$ and $\gamma'=(\gamma_{\rm N_2}+r\gamma_{\rm Ar})/(1+r),$ with r as the pressure ratio $P_{\rm Ar}/P_{\rm N_2}$. At a total pressure $P_{\rm t}$ of 2.6 kPa (typical in our case), the offset shift on $\nu_{\rm Rb}$ is calculated as $\beta'\times P_{\rm t}=3385$ Hz (see Fig. 1 for the measured value).

When the stem temperature $T_{\rm s}$ was fixed (321K), a temperature coefficient value for the cell volume temperature ($T_{\rm v}$) of TC_v = $-1(1) \times 10^{-12}/{\rm K}$ has been achieved at the inversion temperature point (336K) by a linear fit (cf. Fig. 6), and the quadratic TC gives a value of $-4.34 \times 10^{-12}/{\rm K}^2$.

The temperature coefficient was also measured as a function of the stem temperature $T_{\rm s}$ (cf. Fig. 7). At a fixed $T_{\rm v}$ of 336K, we get a slope of $+1.22\times10^{-11}/{\rm K}$. The limits on the clock stability resulting from these temperature coefficients are evaluated and presented in Table II.

The stem TC effect is a factor of ten higher than the cell volume TC effect. The use of buffer gas mixtures helps

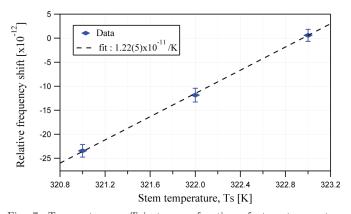


Fig. 7. Temperature coefficient as a function of stem temperature variation. \blacksquare

only to reduce the TC in the cell volume but not for the stem TC. Further studies were done to vindicate the effect caused by the stem TC (see Section V).

E. Spin-Exchange Shift

As explained before, the spin-exchange collisions not only cause the line broadening, they also produce a small phase shift of the oscillating atomic magnetic moment, resulting in an average frequency shift of the clock transition [15], [26], [27], given as

$$\Delta \nu_{\rm SE} = -\frac{1}{8\pi} n \bar{v}_{\rm s} \lambda_{\rm se} \Delta, \tag{6}$$

where $\lambda_{\rm se}$ (= 6.9 × 10⁻¹⁵ cm² for ⁸⁷Rb [26], [27]) is the frequency-shift-related collisional cross-section, and Δ is the population difference between the two hyperfine clock levels [26], [27]. The value and sign of Δ thus depends on the optical pumping condition in which the atomic sample is prepared for clock operation, i.e., whether the optical pumping is done from either 5 $^2S_{1/2}$ $F_{\rm g}=1$ or $F_{\rm g}=2$ [26], [27]. For example, consider that the atoms are pumped from the $F_{\rm g}=1$ state, in which case $\Delta=+1/5$, but if the atoms are pumped from the $F_{\rm g}=2$ state, $\Delta=-1/3$ [26], [27]. The mean velocity between the two colliding Rb atoms with reduced mass μ , inside the cell volume with a temperature $T_{\rm v}$ can be calculated by the formula

$$\overline{v}_{\rm s} = \sqrt{8k_{\rm B} \cdot T_{\rm v}/\pi\mu}, \qquad (7)$$

where $k_{\rm B}$ is the Boltzmann constant.

The spin-exchange frequency shift that is dependent on local temperature of the stem $T_{\rm s}$ in an operating range that changes the atomic density correspondingly can be calculated by the formula [26], [27]

$$TC_{SE} = \frac{\delta\left(\frac{\Delta\nu_{SE}}{\nu_{Rb}}\right)}{\delta T_{s}}.$$
 (8)

At an operating cell volume temperature $T_{\rm v}=336{\rm K},\,\overline{v}_{\rm s}$ $\approx 2.86 \times 10^4 \ \mathrm{cm \cdot s^{-1}}$. At the stem temperature of $T_{\mathrm{s}} =$ 321K, the Rb atomic density $n = 2 \times 10^{11}$ cm⁻³. For the condition in which atoms are pumped from $F_{\rm g}=1$ state, $\Delta = +1/5$. Therefore, with these values in (6), one gets an absolute shift of $\Delta\nu_{\rm SE} \approx -0.3$ Hz or $(\Delta\nu_{\rm SE})/\nu_{\rm Rb} = -4.6$ \times 10⁻¹¹. For the dependence on stem temperatures in our operating range around 321K, we can consider that the Rb density increases by 10% per kelvin, and thus we calculate $TC_{SE} \approx -5 \times 10^{-12}/K$. This value is about a factor of two smaller than the observed stem TC shift of $TC_s =$ 1.22×10^{-11} /K (cf. Fig. 7) and also has an opposite coefficient. We call the observed stem TC effect, which is not due to Rb density changes, the stem fast effect and analyze it by attributing it to the geometrical effect of the cell and stem as discussed and quantified in Section V.

F. Cavity Pulling Shift

In a DR-based Rb standard, the vapor cell containing the atoms and buffer gases is placed inside a microwave cavity. Because of the feedback of the cavity on the atoms, any detuning $\Delta\nu_{\rm c}$ of the cavity from $\nu_{\rm Rb}$ causes a cavity pulling effect. The cavity pulling shift can therefore be written as [14]

$$\Delta\nu_{\rm CP} \approx \frac{Q_{\rm c}}{Q_{\rm a}} \frac{C}{(1+S)} \Delta\nu_{\rm c}, \tag{9}$$

where Q_c is the quality factor of the cavity, and $Q_a = \nu_{\rm Rb}/(\Delta\nu_{1/2})$ is the atomic quality factor with the DR signal full-width at half-maximum $\Delta\nu_{1/2}$. $C \approx 10^{-2}$ [14] is a parameter dependent on oscillation threshold, S=2 is the saturation parameter for which the discriminator slope D is maximum, and $\Delta\nu_c$ is a function of temperature. Therefore, if the temperature varies, the cavity frequency also shifts, and so does $\Delta\nu_c$, which implies that $\Delta\nu_{\rm CP}$ changes accordingly, influencing the clock frequency.

For our magnetron-type cavity used in this work, we measured a Q-factor of ≈ 185 [9] for the loaded cavity (after a few months of continuous operation), and the atomic Q-factor $Q_a \approx 2 \times 10^7$ (from Fig. 1). There might be a degradation of cavity-Q because of migration of metallic Rb [28], but this effect was not studied here. The measured temperature sensitivity shift of the cavity's resonance frequency is $(\Delta \nu_c)/(\Delta T) < +7$ kHz/K. Therefore, the temperature dependent cavity pulling shift is estimated to be $(\Delta \nu_{\rm CP})/(\Delta T) \leq 3.2 \times 10^{-14}/{\rm K}$.

G. Medium- to Long-Term Perturbations Summary and Contribution on Clock Instability

In Table II, all the preceding detailed perturbing effects are summarized along with their contributions to the clock's medium- to long-term instability at 10^4 s.

From Table II, it is clear that presently the limiting perturbations in reaching the level of 1×10^{-14} (equivalent to reach a timing accuracy <1 ns/day) are the frequency LS effect $|\beta|$ and the stem TC $|\text{TC}_{\rm s}|$. It is possible to reduce the effect of $|\beta|$ on clock frequency instability by operating our clock at lower input light intensities as explained in Section IV-B. However, we found that the stem TC arises because of our vapor cell geometric effect, as explained in Section V.

V. Vapor Cell Geometric Effects

A. Stem Fast Effect

As mentioned in Section II, our Rb cell has two distinct parts; the cell volume, where the $^{87}{\rm Rb}$ vapor is interrogated with laser and microwave to get the DR signal, and the cell stem that acts as reservoir for metallic Rb, as shown

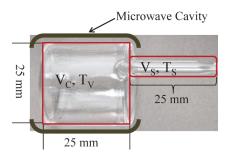


Fig. 8. Vapor cell filled with $^{87}\mathrm{Rb}$ and mixture of buffer gases. The stem serves as reservoir for metallic Rb. The cell volume, V_{c} , where $^{87}\mathrm{Rb}$ vapor interacts with laser and microwave radiation is situated inside a microwave cavity resonator.

in Fig. 8. The stem is also useful to better control the density of Rb inside the cell volume, and helps to increase the operational lifetime of the clock.

As pointed out recently by Calosso et al. [29], a simple model of the ideal gas law suggests that the temperature fluctuations in the stem result in redistribution of buffer gas particles in the entire cell; they call this effect enhanced temperature sensitivity (ETS). This effect is due to the buffer gas density redistribution between the cell body and the stem volumes, which is purely a geometrical effect. The stem part stays outside the microwave cavity, and hence does not contribute in the microwave interrogation. In other words, one can say that the temperature gradient between the cell volume and the stem is responsible for this geometric effect. We quantify this fast stem effect according to [29] as

$$\frac{\partial \nu_{\rm s}/\nu_{\rm Rb}}{\partial T_{\rm s}} = \frac{n_{\rm s}a_0'}{\nu_{\rm Rb}'} \cdot \frac{v_{\rm s}}{T_{\rm s}},\tag{10}$$

where the total volume of the cell (including stem and cell body) is given as $V=V_{\rm s}+V_{\rm c}$, defining $v_{\rm s}=V_{\rm s}/V$ and the average buffer gas density $n_{\rm s}=N/V$. $\nu_{\rm s}$ is the fast shift of clock frequency, in hertz. $\nu'_{\rm Rb}$ is the center frequency of the DR signal. $T_{\rm s}$ is the stem operational temperature. In our case, at the cell filling temperature of 293K with a total buffer gas pressure of 2.6 kPa, we have $n_{\rm s}\approx 1.5\times 10^{17}/{\rm cm}^3$ and $v_{\rm s}=0.029$. From [29], the a'_0 , denotes the buffer gas mixture in the cell volume and is related to β' coefficient in (5) and is estimated as $\approx 5\times 10^{-15}~{\rm Hz\cdot cm}^3$.

Using these values in (10), we obtain $\partial(\nu_{\rm s}/\nu_{\rm Rb})/\partial T_{\rm s} \approx 1.1 \times 10^{-11}/{\rm K}$, in good agreement with the measured value of stem temperature coefficient TC_s (cf. Fig. 7). It is clear from (10) that by reducing the stem volume $\nu_{\rm s}$ (e.g., the reservoir length), one can reduce the fast stem effect, as also was pointed out in [29].

An experimental validation of the fast stem effect is shown in Fig. 9. It is evident that by changing the stem temperature, $T_{\rm s}$, the clock frequency is affected, but the ⁸⁷Rb density in the clock cell (measured by the dc detector voltage in Fig. 9) does not change significantly (here by <0.1%). If the observed frequency shift was due to a

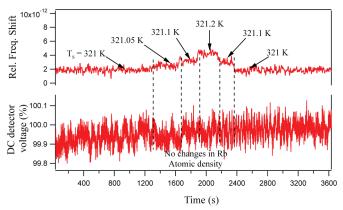


Fig. 9. Impact of changes in $T_{\rm s}$ on clock frequency. Dashed vertical lines represent the times at which the temperature of the stem was changed. Note that there is no effect on the laser intensity passing through the clock cell (denoted the dc detector voltage level, with 100% corresponding to 378 mV here). During these measurements, $T_{\rm v}$ was kept constant.

temperature-related change in Rb density (of 10%/K, see Section IV-E), one would expect to also observe an approximately 2% change in detector voltage, which is not the case here.

Note that in [29], Calosso *et al.* operate their physics package under vacuum in well-controlled laboratory conditions; the stability level of their active temperature control is 100 μ K, whereas in our case (in air, or ambient laboratory conditions) this was measured to be 4.6 mK (a factor of 46 higher).

B. Stem Slow Effect

Further investigation was done to quantify the effect of stem temperature on the clock frequency instability over a period of one day or more. By keeping the cell volume temperature $T_{\rm v}$ constant at 336K, the stem temperature $T_{\rm s}$ was changed from 330K to 323K and the transmitted intensity through the clock cell along with the clock frequency were recorded (cf. Fig. 10). The fast (almost instantaneous) and the slow (over one day) stem temperature coefficients are clearly demonstrated, where, for instance, the light-shift and the microwave power shift related effects are roughly one order of magnitude smaller than the observed clock frequency changes. The fast stem effect is due to stem geometric influence, as discussed in Section V-A.

In Fig. 10, note the absence of the fast effect in dc detector voltage, substantiating that there is no fast change in Rb atomic density in the cell volume after a change in stem temperature $T_{\rm s}$, thus indicating that this effect is due to buffer gas atoms. After the initial temperature step, the negative offset in clock frequency caused by the fast effect persists, but is slowly compensated by the slow effect that shows a frequency change of opposite sign. The fast effect also contributes residual frequency variations on the level of $<10^{-13}$ resulting from temperature fluctuations in our setup of $\delta T_{\rm s} \approx 5$ mK at timescales up to

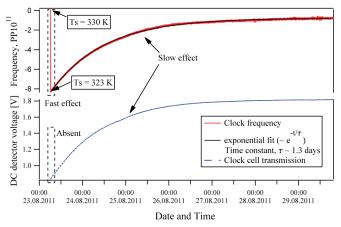


Fig. 10. Clock frequency and transmitted light through the clock cell, after a temperature step of the resonance cell stem. The fast and slow stem effects are demonstrated. The slow stem effect has a time constant of 1.3 d. Note the absence of the fast effect in dc detector voltage substantiating that there is no fast change in Rb atomic density in the cell volume.

few hours (cf. Table II and Section VI). However, these variations are 3 orders of magnitude smaller than the applied temperature step and resulting frequency excursion, and thus are not visible in Fig. 10. The slow stem effect has a time constant of ~ 1.3 d (30 h) and for any change in stem temperature, the Rb atomic density in the cell volume takes about 4 d to reach equilibrium. In our clock conditions, an ultimate steady state is hardly ever reached because of faster (though small) thermal fluctuations on the stem temperature control, such as diurnal cycles. The effect shown in Fig. 10 over a period of 1 d timescale can thus have an influence on the clock frequency stability, by influencing the density of the Rb atoms in the cell. The clock stability limitations resulting from the slow and fast effect could be improved by 1) improved stem temperature control and/or 2) a better thermal isolation of the PP (for example, by operating the PP inside a vacuum chamber).

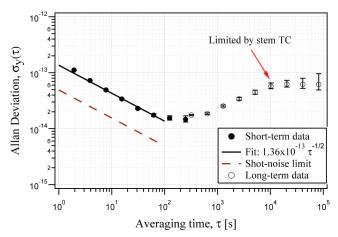


Fig. 11. All an deviation showing the clock's short-term stability of 1.36 \times $10^{-13}~\tau^{-1/2}$ and a shot-noise limit of 4.9 \times $10^{-14}~\tau^{-1/2}.$ The limit resulting from stem TC on medium- to long-term time scales around 5.5 \times 10^{-14} is seen.

VI. MEASURED CLOCK STABILITY

Our clock was operated in typical ambient laboratory conditions, in air and not under vacuum. Fig. 11 shows the measured short-term frequency data in terms of Allan deviation, exhibiting a stability level of $1.36 \times 10^{-13} \, \tau^{1/2}$. At longer integration times, stability is limited at 10^4 s to $5.7(6) \times 10^{-14}$. This is in excellent agreement with the estimated limit resulting from the stem temperature coefficient, $|TC_s|$ (see Table II), which is attributed to the cell's geometric effect. A small linear drift of $+1.2 \times 10^{-13}/{\rm day}$ has been removed.

VII. CONCLUSIONS

We have presented the performance evaluation of a high-performance CW DR clock, using a Rb buffer gas cell in a custom-designed microwave resonator cavity. DR spectroscopic and metrological studies affecting the clock's medium- to long-term frequency stability were presented. The combined volume of our LH and PP is <1.7 dm³, with a total mass of <2 kg. Our clock exhibits S/N-limited short-term stability of <1.4 \times 10⁻¹³ $\tau^{1/2}$, this is in agreement with the estimated short-term noise budget, whose main limitation arises from the laser noise.

Metrological studies on medium- to long-term perturbing effects were studied in detail and were presented. The microwave power shift and its dependence on laser intensity, especially at reduced LS coefficient condition, was demonstrated. We have shown that the frequency LS coefficient (β) could be reduced by operating at lower laser input intensities. The clock's stability at 10^4 integration time is presently limited around 5.5×10^{-14} because of the stem TC, which is characterized as the vapor cell geometric effect. By reducing the volume of the stem, we foresee minimization of the geometric effect; furthermore, by operating our PP under vacuum we could reach stability levels below 1×10^{-14} as demonstrated for the pulsed-optical-pumping (POP) clock [3], but without the need for pulsed operation.

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